PART 3 CHAPTER 4

STABILITY AND WATERTIGHT INTEGRITY

JULY 1995

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CHANGES IN THE RULES

General

The present edition of the Rules includes additions and amendments decided by the Board as of June 1995, and supersedes the January 1994 edition of the same chapter.

The Rule changes come into force on 1st of January 1996.

This chapter is valid until superseded by a revised chapter. Supplements will not be issued except for minor amendments and an updated list of corrections presented in the introduction booklet. The introduction booklet is normally revised in January and July each year.

Revised chapters will be forwarded to all subscribers to the Rules. Buyers of reprints are advised to check the updated list of Rule chapters printed on the front page to ensure that the chapter is current.

Main changes

- **Sec.3 Design Requirements**

  In Table A1, references with respect to Tankers for Oil, Tankers for Chemicals and Tankers for Liquefied gas have been amended.

Corrections and Clarifications

In addition to the above stated rule amendments, some detected errors have been corrected, and some clarifications have been made in the existing rule wording.

Comments to the rules may be sent by e-mail to rules@dnv.com

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SECTION 1
GENERAL

A. Classification

A 100 Application
101 All vessels are to comply with the stability requirements of this Chapter, as applicable for the main class.
102 The requirements in this Chapter are in compliance with IMO Intact Stability Code (IMO Res. A. 749 (18)) and with relevant regulations of SOLAS Ch.II-1.
103 SOLAS texts directly quoted are printed in Italics. References to SOLAS regulations are given. If any part of the rules are subject to discussion or misunderstanding the SOLAS text shall prevail.
104 For vessels with service restrictions as described in Pt.1 Ch.1 Sec.2 B400, modified stability requirements may be considered if consistent with the applicable service restriction.

A 200 Additional class notations
201 Vessels with additional class notations are to comply with additional stability requirements as given in the appropriate chapters.
202 Ships with loading computer systems intended for stability control are to comply with Sec.2 D100, and will be assigned the additional class notation LCS (I). The letter I in the bracket specifies that the loading computer system is approved for calculation and control of intact stability. If applicable G for grain stability and D for damage stability may be added, i.e. LCS (I G D).

B. Definitions

B 100 Symbols
101 VCG: Vertical Centre of Gravity
GM : Metacentric Height
GZ : Righting Lever

B 200 Terms
201 External watertight integrity
The capability of the hull structure and its external closing appliances to prevent downflooding to volumes assumed buoyant. The external watertight integrity includes position and type of closing appliances, alarms, indicators, remote controls and signboards fitted to such appliances.
202 Weathertight
Weatherproof means that in any sea conditions water will not penetrate into the ship.
203 Watertight
Capable of preventing ingress of water during static submersion under a head of water for which the surrounding structure is designed.
A watertight closing appliance is also considered weathertight.
204 Downflooding
Ingress of water through external openings to buoyancy volumes.
205 Downflooding angle related to intact stability
The minimum heel angle where an external opening without weathertight closing appliance is submerged.

206 Dynamic angle
The angle up to which the requirement to area-under-the-righting- lever-curve is fulfilled. The dynamic angle can not be more than the downflooding angle.
207 Lightweight
Lightweight is the displacement of a ship in tonnes without cargo, fuel, lubricating oil, ballast water, fresh water and feed water in tanks, consumable stores, and passengers and crew and their effects.
The lightweight definition stated in the Stability Manual indicates which items are included or not included in the lightweight.

Guidance note:
The approved lightweight data are the data which are approved for the purpose of stability approval and control but not necessarily for determination of the deadweight.

208 First intercept
The angle of heel where the righting lever curve intercepts the heeling lever curve for the first time.
The first intercept is also known as the «static angle of heel».
209 Second intercept
The angle of heel where the righting lever curve intercepts the heeling lever curve for the second time.
210 Maximum allowable vertical centre of gravity
The maximum vertical centre of gravity of the vessel, corrected for free surface effect, which complies with the stipulated stability requirements for the draught in question.
211 Preliminary stability documentation
The stability documentation which is based on estimated lightweight data.
212 Final stability documentation
The stability documentation which is based on approved lightweight data obtained from an inclining test or lightweight survey.

C. Documentation

C 100 Documentation for approval
101 The following documentation is to be submitted for approval:
— preliminary stability booklet
— inclining test procedure
— inclining test report
— final stability booklet
— flooding effect information for dry cargo ships.

Guidance note:
Refer to IMO MSC/Circ. 434: Guidelines for the preparation of information on the effect of flooding to be provided to masters of dry cargo ships.

102 All stability documentation submitted for approval is to have a unique identification, i.e.:
— name and identity no. of ship...
For each sister vessel, it is sufficient to submit:

- lightweight survey procedure (inclining test procedure for passenger vessels)
- lightweight survey report (or inclining test report for passenger vessels)
- final stability booklet.

If the assignment of class is to be based on the approval of the Flag Administration according to Pt.1 Ch.1 Sec.3 A1200, a copy of the final stability documentation stamped by the Flag Administration and the approval letter issued by the Flag Administration are to be submitted to the Society.

For instrumentation and automation, including computer based control and monitoring, see Pt.4 Ch.9 Sec.1.

The following documentation is to be submitted for information:

- general arrangement
- body plan, lines plan or offset table
- external watertight integrity plan or freeboard plan.

Guidance note:
Details of the documentation in 100 and 200 is given in Classification Note No. 20.1 «Stability Documentation — Ships».

D. Surveys and Tests

D 100 General

The following surveys and tests are to be carried out:

- external watertight integrity survey with respect to unprotected and protected openings together with their closing appliances, alarms, indicators and signboards
- checking of draft marks
- remote draft measurement and tank gauging systems
- inclining test or lightweight survey.
SECTION 2
GENERAL REQUIREMENTS

A. Stability Booklet

A 100 General

101 An approved stability booklet is to be provided onboard. The stability booklet is to include information as is necessary to enable the master by a rapid and simple process to obtain accurate guidance as to the stability of the ship under varying conditions of service.

Guidance note:
The format of the stability booklet and the information included will vary dependent on the ship type and operation, however, the following information should be included as far as applicable:

— a general description of the ship
— instructions on the use of the booklet
— general arrangement plans showing watertight compartments, closures, vents, downflooding angles, permanent ballast, allowable deck loads and freeboard diagrams
— hydrostatic curves or tables and cross curves of stability
— capacity plan or tables showing capacities and centre of gravity for each cargo stowage space
— tank sounding tables showing capacities, centres of gravity and free surface data for each tank
— information on loading restrictions, such as maximum KG or minimum GM curve or table that can be used to determine compliance with the applicable stability criteria
— examples of operating conditions and instructions for developing other acceptable loading conditions
— a brief description of the stability calculations done including assumptions
— general precautions to prevent unintentional flooding
— information concerning the use of any special cross-flooding fittings with description of damage conditions which may require cross-flooding
— any other necessary guidance for the safe operation of the vessel under normal and emergency conditions
— a table of contents and index for each booklet
— inclining test report and lightweight data.

---end---of---Guidance---note---

102 Stability data and associated plans are to include a translation into English, if English is not used as official language.

B. Fixed Ballast

B 100 General

101 If used, fixed ballast is to be installed in a manner that prevents shifting of position.

C. Draught Marks

C 100 General

101 The ship is to have scale of draught marks at the bow and stern on both port and starboard side.

Guidance note:
The draught marks should reflect the extreme draught at the location where they are fitted. The stability manual should contain guidance on, from draught mark readings, how to utilise the stability information contained therein.
Norwegian Standard NS6301 may be referenced for further guidelines on the size and location of draught marks.

---end---of---Guidance---note---

D. Loading Computer System

D 100 General

101 Loading computers for stability calculation are to be considered as supplementary to the approved stability booklet.

102 Loading computers for stability control are to comply with Pt.6 Ch.9.

103 An instruction manual and print-out from the loading computer of four loading conditions taken from the final stability booklet are to be provided onboard for use by the officers.
SECTION 3
DESIGN REQUIREMENTS

A. Intact Stability Criteria

A 100 General stability criteria

101 The following criteria are given for all ships:

— The area under the righting lever curve (GZ curve) is not to be less than 0,055 metre-radians up to $\theta = 30^\circ$ angle of heel and not less than 0,09 metre-radians up to $\theta = 40^\circ$ or the angle of flooding $\theta_f$ if this angle is less than 40°. Additionally, the area under the righting lever curve between the angles of heel of 30° and 40° or between 30° and $\theta_f$, if this angle is less than 40°, is not to be less than 0,03 metre-radians.

— The righting lever (GZ) is to be at least 0,20 m at an angle of heel equal to or greater than 30°.

— The maximum righting lever should occur at an angle of heel preferably exceeding 30° but not less than 25°.

— The initial metacentric height, $GM_o$, is not to be less than 0,15 m.

Guidance note:

For ships carrying timber deck cargoes and provided that:

— the cargo extends longitudinally between superstructures end, or where there is no limiting superstructure at the after end, the timber deck cargo shall extend at least to the after end of the aftermost hatchway

— the cargo extends transversely for the full beam of the ship after due allowance for a rounded gunwale not exceeding 4% of the breadth of the ship

— supporting uprights are secured and remain securely fixed at large angles of heel.

the following criteria may be used instead of the criteria in 101:

— the area under the righting lever curve (GZ curve) should not be less than 0,08 metre-radians up to an angle of 15° when the maximum righting lever (GZ) occurs at 15° and 0,055 metre-radians up to an angle of 30° when the maximum righting lever (GZ) occurs at 30° or above. Where the maximum righting lever (GZ) occurs at angles of between 15° and 30°, the corresponding area under the righting lever curve should be:

$$0,055 + 0,001 (30^\circ - \theta_{\text{max}}) \text{ metre-radians}$$

where $\theta_{\text{max}}$ is the angle of heel in degrees at which the righting lever curve reaches its maximum.

— The area under the righting lever curve (GZ curve) between the angles of heel of 30° and 40°, or between 30° and $\theta_f$ this angle is less than 40°, should be not less than 0,03 metre-radians.

— The righting lever (GZ) should be at least 0,20 m at an angle of heel equal to or greater than 30°.

— The maximum righting lever (GZ) should occur at an angle of heel not less than 15°.

— The initial transverse metacentric height ($GM_o$) should not be less than 0,15 m.

102 The following equivalent criteria are recommended where a vessel’s characteristics render compliance with 101 impracticable (normally applicable for vessels such as supply vessels, tugs, fire fighters) (based on IMO Res. A. 749 (18), Ch.4.5.6):

— The area under the curve of righting levers (GZ curve) should not be less than 0,070 metre-radians up to an angle of 15° when the maximum righting lever (GZ) occurs at 15° and 0,055 metre-radians up to an angle of 30° when the maximum righting lever (GZ) occurs at 30° or above. Where the maximum righting lever (GZ) occurs at angles of between 15° and 30°, the corresponding area under the righting lever curve should be:

$$0,055 + 0,001 (30^\circ - \theta_{\text{max}}) \text{ metre-radians}$$

where $\theta_{\text{max}}$ is the angle of heel in degrees at which the righting lever curve reaches its maximum.

— The area under the righting lever curve (GZ curve) between the angles of heel of 30° and 40°, or between 30° and $\theta_f$ this angle is less than 40°, should be not less than 0,03 metre-radians.

— The righting lever (GZ) should be at least 0,20 m at an angle of heel equal to or greater than 30°.

— The maximum righting lever (GZ) should occur at an angle of heel not less than 15°.

— The initial transverse metacentric height ($GM_o$) should not be less than 0,15 m.

103 When anti-rolling devices are installed in a ship, the applicable intact stability criteria are to be satisfied when the devices are in operation.

104 For certain ship types additional or alternative intact and damage stability criteria have been specified. These vessels (or class notations) are given in Table A1.
For ships with large windage area, such as passenger, container and Ro/Ro ships, the criteria listed below are to be complied with (based on IMO Res. A. 749 (18), Ch.3.2):

1. The ability of a ship to withstand the combined effects of beam wind and rolling should be demonstrated for each standard condition of loading, with reference to the Fig. 1 as follows:

A 200 Weather criterion

1. For ships with large windage area, such as passenger, container and Ro/Ro ships, the criteria listed below are to be complied with (based on IMO Res. A. 749 (18), Ch.3.2):

   1. The ability of a ship to withstand the combined effects of beam wind and rolling should be demonstrated for each standard condition of loading, with reference to the Fig. 1 as follows:

   1.1 - the ship is subjected to a steady wind pressure acting perpendicular to the ship's centreline which results in a steady wind effect on the ship.
wind heeling lever \((l_{w1})\).

1.2 - from the resultant angle of equilibrium \((\theta_0)\), the ship is assumed to roll owing to wave action to an angle of roll \((\theta_1)\) to windward. Attention should be paid to the effect of steady wind so that excessive resultant angles of heel are avoided.

The angle of heel under action of steady wind \((\theta_0)\) should be limited to a certain angle to the satisfaction of the Society. As a guide, 16° or 80% of the angle of deck edge immersion, whichever is less, is suggested.

1.3 - the ship is then subjected to a gust wind pressure which results in a gust wind heeling lever \((l_{w2})\);

1.4 - under these circumstances, area \(b\) should be equal to or greater than area \(a\);

1.5 - free surface effects should be accounted for in the standard conditions of loading as set out in B100.

![Fig. 1 Severe wind and rolling](image)

The angles in Fig. 1 are defined as follows:

\(\theta_0\) = angle of heel under action of steady wind (see 1.2 and 3)

\(\theta_1\) = angle of roll to windward due to wave action

\(\theta_2\) = angle of downflooding \((\theta_f)\) or 50° or \(\theta_c\) whichever is less, where:

\(\theta_f\) = angle of heel at which openings in the hull, superstructures or deckhouses which cannot be closed weather-tight immerse. In applying this criterion, small openings through which progressive flooding cannot take place need not be considered as open.

\(\theta_c\) = angle of second intercept between wind heeling lever \((l_{w2})\) and GZ curves.

2 The wind heeling levers \((l_{w1})\) and \((l_{w2})\) referred to in 1.1 and 1.3 are constant values at all angles of inclination and should be calculated as follows:

\[ l_{w1} = \frac{PAZ}{1000 \ g \ disp} \ (m) \]

\[ l_{w2} = 1.5 l_{w1} \ (m) \]

where:

\(P\) = 504 N/m² (wind speed = 29 m/s). The value of \(P\), used for ships in restricted service and/or for ships with very large windage areas (due to coherence length for wind speed), may be reduced subject to the approval of the Society

\(A\) = projected lateral area of the portion of the ship and deck cargo above the waterline \((m²)\)

\(\theta_1\) = vertical distance from the centre of A to the centre of the underwater lateral area or approximately to a point at one half the draught \((m)\)

\(\text{disp} = \text{displacement} \ (t)\)

\(g = 9.81 \ m/s²\)

The angle of roll \((\theta_1)\) * referred to in 1.2 should be calculated as follows:

\[ \theta_1 = 109kX_1X_2\sqrt{\text{disp}/s} \ (\text{degrees}) \]

* The angle of roll for ships with anti-rolling devices should be determined without taking into account the operation of these devices.

where:

\(X_1 = \text{factor as shown in Table A2}\)

\(X_2 = \text{factor as shown in Table A3}\)

\(k = 1.0 \text{ for round-bilged ship having no bilge or bar keels}\)

\(= 0.7 \text{ for a ship having sharp bilges}\)

\(= \text{as shown in Table A4 for a ship having bilge keels, a bar keel or both}\)

\(r = 0.73 \pm 0.6 \text{ OG/d, with:}\)

\(\text{OG} = \text{distance between the centre of gravity and the waterline (m)}\)

\(d = \text{mean moulded draught of the ship (m)}\)

\(s = \text{factor as shown in Table A5.}\)

Table A2 Values of factor \(X_1\)

<table>
<thead>
<tr>
<th>(B/d)</th>
<th>(X_1)</th>
</tr>
</thead>
<tbody>
<tr>
<td>(\leq 2.4)</td>
<td>1.0</td>
</tr>
<tr>
<td>2.5</td>
<td>0.98</td>
</tr>
<tr>
<td>2.6</td>
<td>0.96</td>
</tr>
<tr>
<td>2.7</td>
<td>0.95</td>
</tr>
<tr>
<td>2.8</td>
<td>0.93</td>
</tr>
<tr>
<td>2.9</td>
<td>0.91</td>
</tr>
<tr>
<td>3.0</td>
<td>0.90</td>
</tr>
<tr>
<td>3.1</td>
<td>0.89</td>
</tr>
<tr>
<td>3.2</td>
<td>0.88</td>
</tr>
<tr>
<td>3.3</td>
<td>0.87</td>
</tr>
<tr>
<td>3.4</td>
<td>0.86</td>
</tr>
<tr>
<td>(\geq 3.5)</td>
<td>0.85</td>
</tr>
</tbody>
</table>

Table A3 Values of factor \(X_2\)

<table>
<thead>
<tr>
<th>(C_b)</th>
<th>(X_2)</th>
</tr>
</thead>
<tbody>
<tr>
<td>(\leq 0.45)</td>
<td>0.75</td>
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<tr>
<td>0.50</td>
<td>0.82</td>
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<tr>
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</tr>
<tr>
<td>0.60</td>
<td>0.95</td>
</tr>
<tr>
<td>0.65</td>
<td>0.97</td>
</tr>
<tr>
<td>(\geq 0.70)</td>
<td>1.0</td>
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</tbody>
</table>

Table A4 Values of factor \(k\)

<table>
<thead>
<tr>
<th>(A_1 100)</th>
<th>(k)</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>1.05</td>
</tr>
<tr>
<td>1.0</td>
<td>0.98</td>
</tr>
<tr>
<td>1.5</td>
<td>0.95</td>
</tr>
<tr>
<td>2.0</td>
<td>0.88</td>
</tr>
<tr>
<td>2.5</td>
<td>0.79</td>
</tr>
<tr>
<td>3.0</td>
<td>0.74</td>
</tr>
<tr>
<td>3.5</td>
<td>0.72</td>
</tr>
<tr>
<td>(\geq 4.0)</td>
<td>0.70</td>
</tr>
</tbody>
</table>
(Intermediate values in Tables A2 to A5 should be obtained by linear interpolation).

Rolling period

\[ T = \frac{2CB}{\sqrt{GM}} \] (seconds)

where:

- \( C = 0.373 + 0.023 (B/d) - 0.043 (L/100) \)

The symbols in Tables A2 to A5 and the formula for the rolling period are defined as follows:

- \( L \) = waterline length of the ship (m)
- \( B \) = moulded breadth of the ship (m)
- \( d \) = mean moulded draught of the ship (m)
- \( C_b \) = block coefficient
- \( A_k \) = total overall area of bilge keels, or area of the lateral projection of the bar keel, or sum of these areas (m²)
- \( GM \) = metacentric height corrected for free surface effect (m).

**202** Other calculation methods of equivalent safety level may be accepted as an alternative to the above.

### B. Free Surface of Liquid in Tanks

**B 100 General**

**101** For all loading conditions in C the initial metacentric height and the stability curves are to be corrected for the effect of free surface of liquid in tanks.

**102** Single tanks or combination of tanks for each kind of liquid, including those for water ballast, which according to the loading conditions can simultaneously have free surfaces, are to be considered when correcting for the effect of free surface.

**Guidance note:**

For the purpose of determining the free surface correction, the tanks assumed slack should be those which develop the greatest free surface moment at 30 degrees inclination when in the 50% full condition. Small tanks, for which the free surface correction according to the preceding is less than 0.01 metre at the minimum ship displacement, need not be included in the calculations. The usual remainder of liquids in empty tanks need not be taken into account.

---end---of---Guidance---note---

### C. Loading Conditions

**C 100 General**

**101** Compliance with the stability criteria is to be checked for the main loading conditions intended by the owner in respect of the vessel's operation.

**102** If the owner does not supply sufficiently detailed information regarding such loading conditions, calculations are to be made for the standard loading conditions in C200.

**C 200 Standard loading conditions**

**201** The following standard loading conditions apply to cargo ships:

- ship in the fully loaded departure condition, with cargo homogeneously distributed throughout all cargo spaces and with full stores and fuel
- ship in the fully loaded arrival condition, with cargo homogeneously distributed throughout all cargo spaces and with 10% stores and fuel remaining
- ship in ballast in departure condition, without cargo but with full stores and fuel
- ship in ballast in arrival condition, without cargo and with 10% stores and fuel remaining.

**202** The following additional loading conditions apply to cargo ships intended to carry deck cargoes:

- ship in the fully loaded departure condition with cargo homogeneously distributed in the holds and with cargo specified in extension and weight on deck, with full stores and fuel
- ship in the fully loaded arrival condition with cargo homogeneously distributed in the holds and with cargo specified in extension and weight on deck, with 10% stores and fuel.

**Guidance note:**

The loading conditions in 201 (and 202, if applicable) should be calculated regardless of conditions specified as a consequence of 101.

---end---of---Guidance---note---

**203** If a dry cargo ship has tanks for liquid cargo, the effective deadweight in the fully loaded conditions in 201 and 202 is to be distributed according to two assumptions, i.e. with cargo tanks full, and with cargo tanks empty.

**204** In the fully loaded departure conditions in 201 and 202 the ship is to be assumed loaded to the summer load waterline, or if intended to carry timber deck cargo, to the summer timber load line. The water ballast tanks should normally be assumed empty.

**205** If in any loading condition water ballast is necessary, the quantity and disposition of the water ballast is to be stated.

**206** In all cases, the cargo in holds is assumed fully homogeneous unless this is inconsistent with the practical service of the ship.

**207** Where timber deck cargoes are carried, the amount of cargo and ballast is to correspond to the worst service condition in which all the stability criteria in A100 are met. In the arrival condition it is to be assumed that the weight of the deck cargo has increased by 10% due to water absorption.

**208** In all cases, when deck cargo is carried, a realistic stowage weight is to be assumed and stated, including the height of the cargo.

**Guidance note:**

For ships carrying timber deck cargoes conditions should be shown indicating the maximum permissible amount of deck cargo having regard to the lightest stowage rate likely to be met in service.

---end---of---Guidance---note---
D. Calculation of Stability

D 100 General

101 Hydrostatic and stability curves (cross curves of stability) are normally to be prepared on a designed trim basis. However, where the operating trim or the form and arrangement of the ship are such that change in trim has an appreciable effect on the hydrostatics or the stability curves, the hydrostatics or the stability curves are to be prepared for the intended range of operating trim. Calculation of stability curves is to be done on a free to trim basis.

D 200 Deckhouses and superstructures

201 Enclosed superstructures complying with Pt.3 Ch.1 Sec.1 B212 b) may be taken into account.

202 The second tier of similarly enclosed superstructures may also be taken into account.

203 Deckhouses on the freeboard deck may be taken into account, provided that they comply with the conditions for enclosed superstructures.

204 Where deckhouses comply with 203, except that no additional exit is provided to a deck above, such deckhouses are not to be taken into account. However, any opening inside such deckhouses are to be considered as closed even where no means of closure are provided.

205 Deckhouses, the doors of which do not comply with Pt.3 Ch.1 Sec.11 B101, is not to be taken into account. However, any opening inside such deckhouses are to be considered as closed even where no means of closure are provided.

206 Deckhouses on decks above the freeboard deck are not to be taken into account, but openings within them may be regarded as closed.

207 Superstructures and deckhouses not regarded as enclosed can, however, be taken into account in stability calculations up to the angle at which their openings are flooded. At this angle, the stability curve should show one or more steps, and in subsequent computations the flooded space is to be considered non-existent.

208 In cases where the ship would sink due to flooding through any openings, the stability curve is to be cut short at the corresponding angle of flooding, and the ship is to be considered to have entirely lost its stability.

209 Small openings such as those for passing wires or chains, tackle and anchors, and also holes of scuppers, discharge and sanitary pipes need not be considered as open if they submerge at an angle of inclination more than 30°. If they submerge at an angle of 30° or less, these openings are to be assumed open if they in the opinion of the Society can be considered as source of significant flooding.

210 Trunks may be taken into account. Hatchways may also be taken into account provided they have efficient closure.

D 300 Effect of timber deck cargo

301 The Society may allow account to be taken in stability calculations of the buoyancy of the deck cargo assuming that such cargo has a permeability of 0.25.

E. Damage Stability of Cargo Ships

E 100 Application

101 Cargo ships over 80 m in length (Lₘ) and upwards are to comply with the damage stability requirements in Pt.5 Ch.2 Sec.8, except those vessels which may be exempted in accordance with Pt.5 Ch.2 Sec.8 A101.
SECTION 4
WATERTIGHT INTEGRITY

A. General

100 General

101 Openings in the shell, exposed decks and in enclosed superstructures and deckhouses which have been taken into account in the stability calculations, are to have closing appliances which comply with the requirements of Ch.2 Sec.11 if the opening may become submerged at an angle of heel less than the dynamic angle.

102 Regulation 23-1
Damage control in dry cargo ships

1 There shall be permanently exhibited or readily available on the navigating bridge, for the guidance of the officer in charge of the ship, a plan showing clearly for each deck and hold the boundaries of the watertight compartments, the openings therein with the means of closure and position of any controls thereof, and the arrangements for the correction of any list due to flooding. In addition, booklets containing the aforementioned information shall be made available to the officers of the ship.

2 Indicators shall be provided for all sliding doors and for hinged doors in watertight bulkheads. Indication showing whether the doors are open or closed shall be given on the navigating bridge. In addition, shell doors and other openings which, in the opinion of the Administration, could lead to major flooding if left open or not properly secured, shall be provided with such indicators.

3.1 General precautions shall consist of a listing of equipment, conditions and operational procedures, considered by the Administration to be necessary to maintain watertight integrity under normal ship operations.

3.2 Specific precautions shall consist of a listing of elements (i.e. closures, security of cargo, sounding of alarms, etc.) considered by the Administration to be vital to the survival of the ship and its crew.

103 The additional indicators and the listing of equipment and elements as prescribed in 102 will be considered by the Society in each case.
SECTION 5
DETERMINATION OF LIGHTWEIGHT DATA

A. Inclining Test

A 100 Application

101 Every passenger ship and cargo ship is to be inclined upon its completion and the lightweight displacement and centre of gravity determined.

102 The inclining test required in 101 may be dispensed with provided basic stability data are available from the inclination test of a sister ship and it is shown to the satisfaction of the Society that reliable stability information for the exempted ship can be obtained from such basic data.

Guidance note:
Dispensation according to 102 is not considered applicable to passenger ships and other ships where the lightweight is more than 75% of the total displacement.

---end---of---Guidance---note---

A 200 Procedure

201 The inclining test is to be carried out according to the approved test procedure and in the presence of the Society’s representative.

Guidance note:
Guidelines for conducting inclining test or lightweight survey are given in Classification Note No. 20.2 «Lightweight Determination — Ships».

---end---of---Guidance---note---

B. Lightweight Survey

B 100 Application

101 A lightweight survey is to be carried out if an inclining test has been dispensed with according to A102.

102 In case structural strength limitations etc. make it impossible to perform an inclining test, a lightweight survey may be accepted provided a detailed lightweight estimate including VCG is worked out in advance and the estimate compared with the result of the lightweight survey. If the lightweight survey reveals a deviation of lightweight data from the estimate, the deviation is to be assumed at the most unfavourable position when calculating the vertical centre of gravity.

B 200 Procedure

201 The lightweight survey is to be carried out according to the approved test procedure and in the presence of the Society’s representative.

Guidance note:
Guidelines for conducting the lightweight survey are given in Classification Note No. 20.2 «Lightweight Determination — Ships».

---end---of---Guidance---note---

202 The lightweight survey report is to be signed by the person responsible for the test and by the Society’s representative.

203 If, compared with the sister ship, the lightweight survey reveals a lightweight displacement deviation exceeding 2% or an LCG deviation exceeding 1% of the length of the ship, an inclining test may be required.

204 The lightweight displacement and the longitudinal centre of gravity obtained by the lightweight survey are to be used in the final stability booklet. If the lightweight displacement deviation is less than 0.5%, the lightweight data of the sister-ship may be used.